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## [CLAIMS]

- [Claim 1] A bake-hardenable cold rolled steel sheet having excellent formability, comprising:  $0.003 \sim 0.005$  % of C;  $0.003 \sim 0.03$  % of S;  $0.01 \sim 0.1$  % of Al; 0.02 % or less of N; 0.2 % or less of P; at least one of  $0.03 \sim 0.2$  % of Mn and  $0.005 \sim 0.2$  % of Cu; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein, when the steel sheet comprises one of Mn and Cu, a composition of Mn, Cu, and S satisfies one of relationships:  $0.58*Mn/S \le 10$  and  $1 \le 0.5*Cu/S \le 10$ , and when the steel sheet comprises both Mn and Cu, a composition of Mn, Cu, and S satisfies the relationships:  $Mn+Cu \le 0.3$  and  $2 \le 0.5*(Mn+Cu)/S \le 20$ , and wherein precipitates of MnS, CuS, and (Mn, Cu)S have an average size of 0.2  $\mu$ m or less.
- [Claim 2] A bake-hardenable cold rolled steel sheet having excellent formability, comprising:  $0.003 \sim 0.005$  % of C;  $0.005 \sim 0.03$  % of S;  $0.01 \sim 0.1$  % of Al; 0.02 % or less of N; 0.2 % or less of P;  $0.05 \sim 0.2$  % of Mn; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein a composition of Mn and S satisfies the relationship:  $0.58*Mn/S \le 10$  in terms of weight, and wherein precipitates of MnS have an average size of  $0.2~\mu m$  or less.
  - [Claim 3] The steel sheet as set forth in claim 2, wherein the steel sheet comprises 0.015 % or less of P.
- [Claim 4] The steel sheet as set forth in claim 2, wherein the steel sheet comprises 0.004 % or less of N.
  - [Claim 5] The steel sheet as set forth in claim 2, wherein the steel sheet comprises  $0.03 \sim 0.2 \%$  of P.
  - [Claim 6] The steel sheet as set forth in claim 2, wherein the steel sheet further comprises at least one of  $0.1 \sim 0.8$  % of Si, and  $0.2 \sim 1.2$  % of Cr.
- 25 [Claim 7] The steel sheet as set forth in claim 2, wherein the steel sheet comprises

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- $0.005 \sim 0.02$  % of N, and  $0.03 \sim 0.06$  % of P.
- [Claim 8] The steel sheet as set forth in claim 7, wherein a composition of Al and N satisfies the relationship:  $1 \le 0.52 \text{ Al/N} \le 5$ .
- [Claim 9] The steel sheet as set forth in any one of claims 2 to 8, wherein the steel sheet further comprises  $0.01 \sim 0.2 \%$  of Mo.
  - [Claim 10] A bake-hardenable cold rolled steel sheet having excellent formability, comprising:  $0.003 \sim 0.005$  % of C;  $0.003 \sim 0.025$  % of S;  $0.01 \sim 0.08$  % of Al; 0.02 % or less of N; 0.2 % or less of P;  $0.01 \sim 0.2$  % of Cu; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein a composition of Cu and S satisfies the relationship:  $1 \le 0.5$ \*Cu/S  $\le 10$  in terms of weight, and wherein precipitates of CuS have an average size of 0.1  $\mu$ m or less.
  - [Claim 11] The steel sheet as set forth in claim 10, wherein the steel sheet comprises 0.015 % or less of P.
- [Claim 12] The steel sheet as set forth in claim 10, wherein the steel sheet comprises 0.004 % or less of N.
  - [Claim 13] The steel sheet as set forth in claim 10, wherein the composition of Cu and S satisfies the relationship:  $1 \le 0.5*Cu/S \le 3$ .
  - [Claim 14] The steel sheet as set forth in claim 10, wherein the steel sheet comprises  $0.03 \sim 0.2 \%$  of P.
- [Claim 15] The steel sheet as set forth in claim 10, wherein the steel sheet further comprises at least one of  $0.1 \sim 0.8$  % of Si, and  $0.2 \sim 1.2$  % of Cr.
  - [Claim 16] The steel sheet as set forth in claim 10, wherein the steel sheet comprises  $0.005 \sim 0.02 \%$  of N, and  $0.03 \sim 0.06 \%$  of P.

- [Claim 17] The steel sheet as set forth in claim 16, wherein a composition of Al and N satisfies the relationship: 1≤0.52\*Al/N≤5.
- [Claim 18] The steel sheet as set forth in any one of claims 10 to 17, wherein the steel sheet further comprises  $0.01 \sim 0.2$  % of Mo.
- [Claim 19] A bake-hardenable cold rolled steel sheet having excellent formability, comprising: 0.003 ~ 0.005 % of C; 0.003 ~ 0.025 % of S; 0.01 ~ 0.08 % of Al; 0.02 % or less of N; 0.2 % or less of P; 0.03 ~ 0.2 % of Mn; 0.005 ~ 0.2 % of Cu; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein a composition of Mn, Cu, and S satisfies the relationships: Mn+Cu≤0.3 and 2≤0.5\*(Mn+Cu)/S≤20 in terms of weight, and wherein precipitates of MnS, CuS, and (Mn, Cu)S have an average size of 0.2 μm or less.
  - [Claim 20] The steel sheet as set forth in claim 19, wherein the steel sheet comprises 0.015 % or less of P.
- [Claim 21] The steel sheet as set forth in claim 19, wherein the steel sheet comprises 0.004 % or less of N.
  - [Claim 22] The steel sheet as set forth in claim 19, wherein the number of precipitates is  $2x10^6$  or more per unit area (mm<sup>2</sup>).
  - [Claim 23] The steel sheet as set forth in claim 19, wherein the composition of Mn, Cu and S satisfies the relationship:  $2 \le 0.5*(Mn+Cu)/S \le 7$ .
- [Claim 24] The steel sheet as set forth in claim 23, wherein the number of precipitates is  $2x10^8$  or more per unit area (mm<sup>2</sup>).
  - [Claim 25] The steel sheet as set forth in claim 19, wherein the steel sheet comprises  $0.03 \sim 0.2 \%$  of P.

- [Claim 26] The steel sheet as set forth in claim 19, wherein the steel sheet further comprises at least one of  $0.1 \sim 0.8$  % of Si, and  $0.2 \sim 1.2$  % of Cr.
- [Claim 27] The steel sheet as set forth in claim 19, wherein the steel sheet comprises  $0.005 \sim 0.02$  % of N, and  $0.03 \sim 0.06$  % of P.
- 5 [Claim 28] The steel sheet as set forth in claim 27, wherein a composition of Al and N satisfies the relationship: 1≤0.52\*Al/N≤5.
  - [Claim 29] The steel sheet as set forth in any one of claims 19 to 28, wherein the steel sheet further comprises  $0.01 \sim 0.2 \%$  of Mo.
- [Claim 30] A method of manufacturing a bake-hardenable cold rolled steel sheet having excellent formability, comprising the steps of: hot-rolling a steel slab with finish rolling at an Ar<sub>3</sub> transformation temperature or more to provide a hot rolled steel sheet, after reheating the steel slab to a temperature of 1,100 °C or more, the steel slab comprising comprising: 0.003 ~ 0.005 % of C; 0.005 ~ 0.03 % of S; 0.01 ~ 0.1 % of Al; 0.02 % or less of N; 0.2 % or less of P; 0.05 ~ 0.2 % of Mn; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein a composition of Mn and S satisfies the relationship: 0.58\*Mn/S≤10 in terms of weight; cooling the steel sheet at a speed of 200 °C/min or more; winding the cooled steel sheet at a temperature of 700 °C or less; cold rolling the steel sheet; and continuous annealing the cold rolled steel sheet.
- [Claim 31] The method as set forth in claim 30, wherein the steel slab comprises 0.015 % or less of P.
  - [Claim 32] The method as set forth in claim 30, wherein the steel slab comprises 0.004 % or less of N.
  - [Claim 33] The method as set forth in claim 30, wherein the steel slab comprises  $0.03 \sim 0.2 \%$  of P.

- [Claim 34] The method as set forth in claim 30, wherein the steel slab further comprises at least one of  $0.1 \sim 0.8$  % of Si, and  $0.2 \sim 1.2$  % of Cr.
- [Claim 35] The method as set forth in claim 30, wherein the steel slab comprises  $0.005 \sim 0.02$  % of N, and  $0.03 \sim 0.06$  % of P.
- 5 [Claim 36] The method as set forth in claim 30, wherein a composition of Al and N satisfies the relationship: 1≤0.52\*Al/N≤5.
  - [Claim 37] The steel sheet as set forth in any one of claims 30 to 36, wherein the steel slab further comprises  $0.01 \sim 0.2$  % of Mo.
- [Claim 38] A method of manufacturing a bake-hardenable cold rolled steel sheet having excellent formability, comprising the steps of: hot-rolling a steel slab with finish rolling at an Ar₃ transformation temperature or more to provide a hot rolled steel sheet, after reheating the steel slab to a temperature of 1,100 °C or more, the steel slab comprising: 0.003 ~ 0.005 % of C; 0.003 ~ 0.025 % of S; 0.01 ~ 0.08 % of Al; 0.02 % or less of N; 0.2 % or less of P; 0.01 ~ 0.2 % of Cu; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein a composition of Cu and S satisfies the relationship: 1≤0.5\*Cu/S≤10 in terms of weight; cooling the steel sheet at a speed of 300 °C/min or more; winding the cooled steel sheet at a temperature of 700 °C or less; cold rolling the steel sheet; and continuous annealing the cold rolled steel sheet.
- [Claim 39] The method as set forth in claim 38, wherein the steel slab comprises 0.015% or less of P.
  - [Claim 40] The method as set forth in claim 38, wherein the steel slab comprises 0.004 % or less of N.
- [Claim 41] The method as set forth in claim 38, wherein the composition of Cu and S satisfies the relationship:  $1 \le 0.5*Cu/S \le 3$ .

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- [Claim 42] The method as set forth in claim 38, wherein the steel slab comprises  $0.03 \sim 0.2\%$  of P.
- [Claim 43] The method as set forth in claim 38, wherein the steel slab further comprises at least one of  $0.1 \sim 0.8$  % of Si, and  $0.2 \sim 1.2$  % of Cr.
- [Claim 44] The method as set forth in claim 38, wherein the steel slab comprises  $0.005 \sim 0.02 \%$  of N, and  $0.03 \sim 0.06 \%$  of P.
  - [Claim 45] The method as set forth in claim 38, wherein a composition of Al and N satisfies the relationship:  $1 \le 0.52 \text{ Al/N} \le 5$ .
- [Claim 46] The method as set forth in any one of claims 38 to 45, wherein the steel slab further comprises  $0.01 \sim 0.2$  % of Mo.
  - [Claim 47] A method of manufacturing a bake-hardenable cold rolled steel sheet having excellent formability, comprising the steps of: hot-rolling a steel slab with finish rolling at an Ar<sub>3</sub> transformation temperature or more to provide a hot rolled steel sheet, after reheating the steel slab to a temperature of  $1,100\,^{\circ}$ C or more, the steel slab comprising:  $0.003 \sim 0.005\,\%$  of C;  $0.003 \sim 0.025\,\%$  of S;  $0.01 \sim 0.08\,\%$  of Al;  $0.02\,\%$  or less of N;  $0.2\,\%$  or less of P;  $0.03 \sim 0.2\,\%$  of Mn;  $0.005 \sim 0.2\,\%$  of Cu; and the balance of Fe and other unavoidable impurities, in terms of weight%, wherein a composition of Mn, Cu, and S satisfies the relationships: Mn+Cu  $\leq 0.3\,$  and  $2 \leq 0.5*(Mn+Cu)/S \leq 20\,$  in terms of weight; cooling the steel sheet at a speed of 300  $^{\circ}$ C/min or more; winding the cooled steel sheet at a temperature of 700  $^{\circ}$ C or less; cold rolling the steel sheet; and continuous annealing the cold rolled steel sheet.
  - [Claim 48] The method as set forth in claim 47, wherein the steel slab comprises 0.015 % or less of P.
- [Claim 49] The method as set forth in claim 47, wherein the steel slab comprises 0.004 % or less of N.

- [Claim 50] The method as set forth in claim 47, wherein the number of precipitates is  $2x10^6$  or more per unit area (mm<sup>2</sup>).
- [Claim 51] The method as set forth in claim 47, wherein the composition of Mn, Cu and S satisfies the relationship:  $2 \le 0.5*(Mn+Cu)/S \le 7$ .
- [Claim 52] The method as set forth in claim 51, wherein the number of precipitates is  $2x10^8$  or more per unit area (mm<sup>2</sup>).
  - [Claim 53] The method as set forth in claim 47, wherein the steel slab comprises  $0.03 \sim 0.2 \%$  of P.
- [Claim 54] The method as set forth in claim 47, wherein the steel slab further comprises at least one of  $0.1 \sim 0.8$  % of Si, and  $0.2 \sim 1.2$  % of Cr.
  - [Claim 55] The method as set forth in claim 47, wherein the steel slab comprises  $0.005 \sim 0.02$  % of N, and  $0.03 \sim 0.06$  % of P.
  - [Claim 56] The method as set forth in claim 55, wherein a composition of Al and N satisfies the relationship:  $1 \le 0.52 * Al/N \le 5$ .
- [Claim 57] The method as set forth in any one of claims 47 to 56, wherein the steel slab further comprises  $0.01 \sim 0.2 \%$  of Mo.